

2.19 Differentiate $(\mathbf{x} - \mathbf{y})^2 = (\mathbf{f}(\mathbf{x}) - \mathbf{f}(\mathbf{y}))^2$ after \mathbf{x} to obtain $\mathbf{x} - \mathbf{y} = (\mathbf{f}(\mathbf{x}) - \mathbf{f}(\mathbf{y})) \cdot \mathbf{a}(\mathbf{x})$ with $\mathbf{a}(\mathbf{x}) = \partial \mathbf{f}(\mathbf{x}) / \partial \mathbf{x}$. Differentiate again after \mathbf{y} to obtain $-\mathbf{1} = -\mathbf{a}(\mathbf{y})^\top \cdot \mathbf{a}(\mathbf{x})$. This means that $\mathbf{a}(\mathbf{x})^{-1} = \mathbf{a}(\mathbf{y})^\top$. The left hand side depends only on \mathbf{x} and the right hand side only on \mathbf{y} which implies that both sides are independent of \mathbf{x} and \mathbf{y} , *i.e.* the matrix \mathbf{a} is a constant. Integrating $\partial \mathbf{f}(\mathbf{x}) / \partial \mathbf{x} = \mathbf{a}$ one gets $\mathbf{f}(\mathbf{x}) = \mathbf{a} \cdot \mathbf{x} + \mathbf{b}$.

2.20 Let $\mathbf{a}_z(\phi)$ be the matrix of the simple rotation (2-40) through an angle ϕ around the z -axis. Then the three Euler angles ϕ , θ and ψ determine any rotation matrix as a product $\mathbf{a}_z(\psi) \cdot \mathbf{a}_y(\theta) \cdot \mathbf{a}_z(\phi)$.

3 Gravity

3.2 The centripetal acceleration in a circular orbit must equal the force of gravity, $v^2/r = GM/r^2$ leading to $v = \sqrt{GM/r} = \sqrt{-\Phi}$. At ground level the velocity becomes $v = v_{\text{esc}}/\sqrt{2} = 7.9 \text{ km/s}$ where $v_{\text{esc}} = 11.2 \text{ km/s}$ is the escape velocity.

3.3 Earth's true rotation period $T = T_0 * 364/365$ is a bit shorter than $T_0 = 24 \text{ hours}$ because of the orbital motion which adds one full revolution in one year. Taking $v = \Omega r$ where $\Omega = 2\pi/T$ we find from the equality of centripetal acceleration and gravity that

$$r\Omega^2 = g_0 \frac{a^2}{r^2} . \quad (3-A1)$$

which solved for r/a yields

$$\frac{r}{a} = \left(\frac{g_0}{a\Omega^2} \right)^{1/3} \approx 6.613 . \quad (3-A2)$$

The orbit height is $h = r - a \approx 5.613a \approx 35,800 \text{ km}$.

3.4 At the height z above the ground the force on a small piece dz of the line is

$$d\mathcal{F} = \left(-g_0 \frac{a^2}{(a+z)^2} + (a+z)\Omega^2 \right) \rho A dz \quad (3-A3)$$

where Ω is the angular velocity in the stationary orbit and the second term represents the centrifugal force. Since this only vanishes for $z = h$, the total force is maximal at the satellite. Integrating the force from 0 to h , we find the maximal force

$$\mathcal{F} = \int_0^h d\mathcal{F}(z) = \rho A h \left(-g_0 \frac{a}{a+h} + \Omega^2 \left(a + \frac{1}{2}h \right) \right) . \quad (3-A4)$$

The absolute value of the tension-to-density ratio becomes,

$$\frac{\sigma}{\rho} = h \left(g_0 \frac{a}{a+h} - \Omega^2 \left(a + \frac{1}{2}h \right) \right) \approx 4.8 \times 10^7 \text{ m}^2/\text{s}^2 \quad (3-A5)$$

The tensile strength a Beryllium-Copper alloy of density $\rho = 8230 \text{ kg/m}^3$ can go as high as $\sigma \approx 1.4 \text{ GPa}$, leading to $\sigma/\rho \approx 1.7 \times 10^5 \text{ m}^2/\text{s}^2$, a factor nearly 300 below the required value.

3.7 A small volume is invariant under a rotation $dv' = dv$ and so is the amount of mass contained in it, $dm' = dm$. By the definition (3-1) we have $dm' = \rho'(\mathbf{x}')dv' = dm = \rho(\mathbf{x})dv$ and from that $\rho'(\mathbf{x}') = \rho(\mathbf{x})$.

3.8 The force on a small volume transforms according to $d\mathbf{F}' = \mathbf{a} \cdot d\mathbf{F}$ whereas the mass element is invariant $dm' = dm$. By the definition (3-5) we have $d\mathbf{F}' = \mathbf{g}'(\mathbf{x}') dm' = \mathbf{a} \cdot d\mathbf{F} = \mathbf{a} \cdot \mathbf{g}(\mathbf{x})dm$ and from this $\mathbf{g}'(\mathbf{x}') = \mathbf{a} \cdot \mathbf{g}(\mathbf{x})$.

3.10 Cut out a small sphere $|\mathbf{x}' - \mathbf{x}| \leq a$ around the point \mathbf{x} . Let a be so small that $\rho(\mathbf{x}')$ does not vary appreciably within this sphere. Then we get the contribution to gravity from the small sphere

$$\Delta\mathbf{g}(\mathbf{x}) = -G \int_{|\mathbf{x}' - \mathbf{x}| \leq a} \frac{\mathbf{x} - \mathbf{x}'}{|\mathbf{x} - \mathbf{x}'|^3} \rho(\mathbf{x}') dv' \approx -G\rho(\mathbf{x}) \int_{|\mathbf{x}' - \mathbf{x}| \leq a} \frac{\mathbf{x} - \mathbf{x}'}{|\mathbf{x} - \mathbf{x}'|^3} dv' = \mathbf{0}$$

The last integral vanishes because of the spherical symmetry (it is a vector with no direction to point in).

3.5

- a) Minimal kinetic energy: $\frac{1}{2}v_{\text{esc}}^2 \approx 63 \text{ (km/s)}^2 = 63 \times 10^6 \text{ J/kg}$.
 b) Melting, heating and evaporating ice: $\approx 3 \times 10^6 \text{ J/kg}$.

3.6 Energy conservation: $\frac{1}{2}\dot{r}^2 + \Phi(r) = \Phi(a)$. Use (3-31).

- a) $v_0 = -\dot{r}|_{r=0} = a\sqrt{\frac{4}{3}\pi\rho_0 G} = \sqrt{g_0 a} = 7.9 \text{ km s}^{-1}$.
 b) $t_0 = \int_0^a \frac{dr}{\sqrt{2(\Phi(a) - \Phi(r))}} = \int_0^a \frac{dr}{\sqrt{\frac{4}{3}\pi\rho_0 G(a^2 - r^2)}} = \frac{\pi a}{2v_0} = 1267 \text{ s}$.

3.11 From (3-17) we get

$$g(r) = -\frac{4}{3}\pi G \begin{cases} r\rho_1 & r \leq a_1 \\ \frac{a_1^3}{r^2}\rho_1 + \left(r - \frac{a_1^3}{r^2}\right)\rho_2 & a_1 < r \leq a \\ \frac{a_1^3\rho_1 + (a^3 - a_1^3)\rho_2}{r^2} & r > a \end{cases} \quad (3-A6)$$

and from (3-28)s

$$\Phi(r) = -\frac{2}{3}\pi G \begin{cases} (3a_1^2 - r^2)\rho_1 + 3(a^2 - a_1^2)\rho_2 & r \leq a_1 \\ 2\frac{a_1^3}{r}\rho_1 + \left(3a^2 - r^2 - 2\frac{a_1^3}{r}\right)\rho_2 & a_1 \leq r \leq a \\ 2\frac{a_1^3}{r}\rho_1 + 2\frac{a^3 - a_1^3}{r}\rho_2 & r \geq a \end{cases} \quad (3-A7)$$

3.12 Using the two-layer model it follows from $|g(a_1)| > |g(a)|$, that $a_1\rho_1 > (a_1^3\rho_1 + (a^3 - a_1^3)\rho_2)/a^2$ which may be rewritten in the form of the inequality (3-43). For the Earth the left hand side becomes 1.42 and the right hand side 1.18, so the inequality is fulfilled.

3.13

$$\text{a) } g(r) = -4\pi G \frac{A}{3+\alpha} r^{1+\alpha}, \quad \Phi(r) = 4\pi G \frac{A}{2+\alpha} \left(\frac{r^{2+\alpha}}{3+\alpha} - a^{2+\alpha} \right).$$

$$\text{b) } \alpha > -3.$$

$$\text{c) } -3 < \alpha < -1.$$

3.14 Use eq. (3-17). Setting $u = r/a$ one gets

$$M(r) = \int_0^r \rho(s) 4\pi s^2 ds = 4\pi \rho_0 \int_0^r e^{-s/a} s^2 ds = 4\pi \rho_0 a^3 (2 - (2 + 2u + u^2)e^{-u})$$

Similarly, using (3-30) one finds

$$\int_r^\infty s \rho(s) ds = \rho_0 \int_r^\infty s e^{-s/a} ds = \rho_0 a^2 (1 + u) e^{-u}$$

and from this

$$\Phi = -\frac{4\pi G \rho_0 a^3}{r} (2(1 - e^{-u}) - u e^{-u})$$

3.15 Multiplying (3-13) by $\mathbf{e}_r = \mathbf{x}/r$ and using (3-16) one gets

$$g(r) = -G \int_{|\mathbf{x}'| \leq a} \frac{\mathbf{x} \cdot (\mathbf{x} - \mathbf{x}')}{r |\mathbf{x} - \mathbf{x}'|^3} \rho(\mathbf{x}') dv'$$

Introducing $s = |\mathbf{x}'|$ and the angle θ between \mathbf{x} and \mathbf{x}' , so that $dv' = 2\pi \sin \theta d\theta s^2 ds$, this becomes

$$g(r) = -2\pi G \int_0^a \rho(s) s^2 ds \int_{-1}^1 d \cos \theta \frac{r - s \cos \theta}{(r^2 + s^2 - 2rs \cos \theta)^{\frac{3}{2}}}$$

Integrating over $u = \cos \theta$ one obtains

$$\begin{aligned} & \int_{-1}^1 du \frac{r - su}{(r^2 + s^2 - 2rsu)^{\frac{3}{2}}} = -\frac{\partial}{\partial r} \int_{-1}^1 du \frac{1}{\sqrt{r^2 + s^2 - 2rsu}} \\ & = \frac{\partial}{\partial r} \left[\frac{\sqrt{r^2 + s^2 - 2rsu}}{rs} \right]_{u=-1}^1 = \frac{\partial}{\partial r} \frac{|r-s| - (r+s)}{rs} \\ & = -2 \frac{\partial}{\partial r} \begin{cases} \frac{1}{r} & r > s \\ \frac{1}{s} & r < s \end{cases} = \frac{2}{r^2} \theta(r-s) \end{aligned}$$

which leads to the desired result (3-17).